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正交余弦光栅的衍射场

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摘要: 为了研究正交余弦光栅的衍射场,采用波前相因子判断法并考虑到光栅孔径的影响,对正交余弦光栅的衍射进行了理论分析,得到了正交余弦光栅衍射场所含基元成分,导出了像面波前函数、像面振幅分布函数和光强分布函数,并得出主焦斑的半角宽度。结果表明,该研究可为光栅用于光学信息处理技术提供理论依据。

关键词: 衍射与光栅; 波动光学; 正交余弦光栅; 波前相因子; 衍射场

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Diffraction field of orthogonal cosine-gratings

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Abstract: In order to analyze diffraction field of orthogonal cosine-gratings, it was analyzed based on the method of wave-front phase factors and considering the influence of limited aperture of grating. The phase-front function, amplitude and intensity expressions of the diffraction field were deduced. The amplitude and intensity of light distribution diagram of phase plane were obtained. Finally, the half-angle-width of maximum value in the center was given. This study may further provide a theoretical foundation to analyze diffraction of orthogonal cosine-gratings.

Key words: diffraction and gratings; wave optics; orthogonal cosine-grating; wave-front phase factor; diffraction field

引 言

目前,光滤波技术、超光成像技术、光学信息处理技术等涉及到有限孔径的衍射、选频、成像等问题,而对于有限孔径的近场和远场的研究,常常只能选用一些近似的方法来处理问题,例如用半波带法和矢量法,半定性、半定量地分析问题^[1]。因此,有一些定量结果无法得到。本研究是在惠更斯-菲涅耳原理的基础上,用波前相因子判断法对正交余弦光栅的近场和远场进行研究,使问题更加严密直观。

1 波前相因子判断法

一个衍射系统如图 1 所示,其中 $\tilde{U}_1(x_0, y_0, \rho)$ 为入射光波到达衍射屏的波前函数, $\tilde{U}_2(x_0, y_0, \rho)$ 是衍射屏的后场初端的波前函数, $\tilde{U}(x, y, z)$ 是接收屏的

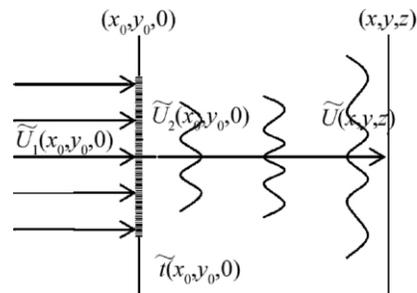


Fig. 1 Diffraction field

波前函数。入射光波前 $\tilde{U}_1(x_0, y_0, \rho)$ 被衍射屏变成出射光波前 $\tilde{U}_2(x_0, y_0, \rho)$, 是衍射屏的作用,由其屏函数 $\tilde{t}(x_0, y_0, \rho)$ 来决定;出射光波前 $\tilde{U}_2(x_0, y_0, \rho)$ 沿传播方向到某处的波前 $\tilde{U}(x, y, z)$ 是波衍射的问题,原则上来说,衍射波的波前可以根据菲涅耳-基尔霍夫衍射积分公式得出,然而这种积分运算相当复杂。如果能把复杂的衍射波看成若干平面波和球面波的组合,使复杂问题变成简单波场的叠加,再用菲涅耳-基尔霍夫衍射积分公式导出衍射波的波前 $\tilde{U}(x, y, z)$ 就简单多了。

所谓波前相因子判断法,就是根据波前函数的相因子,判断波的主要成分,分析衍射波的主要特征,再用菲涅耳-基尔霍夫衍射积分公式计算衍射波的波前 $\tilde{U}(x, y, z)$ 。

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2 正交余弦光栅

当两张余弦光栅紧密地叠放在一起,其条纹正交,称之为正交余弦光栅。如图 2 所示,两张余弦光栅 G_1 和 G_2 其栅纹垂直叠放在一起。

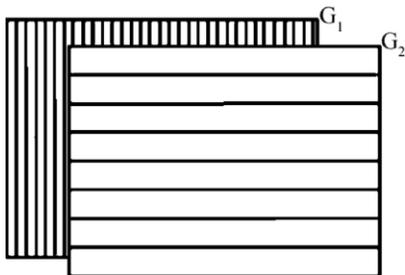


Fig. 2 Orthogonal cosine-gratings

G_1 和 G_2 衍射屏函数的形式分别为:

$$G_1: \tilde{t}_{01}(x_0) = t_{01} + t_1 \cos(2\pi f_1 x_0 + \varphi_0) \quad (1)$$

$$G_2: \tilde{t}_{02}''(y_0) = t_{02} + t_2 \cos(2\pi f_2 y_0 + \varphi_0') \quad (2)$$

3 正交余弦光栅夫琅禾费衍射场

正交余弦光栅夫琅禾费衍射的实验装置如图 3 所示。用平行光照射正交余弦光栅,在透镜的后焦面上接收到的衍射是一个 2 维衍射场。

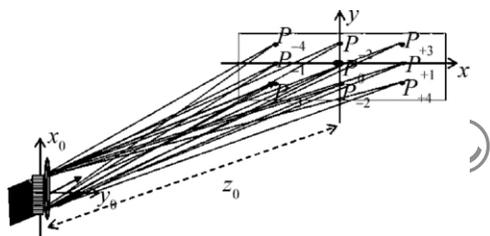


Fig. 3 Diffraction fields of orthogonal cosine-gratings

当正交余弦光栅为一个衍射屏时,则其屏函数为:

$$\begin{aligned} \tilde{t}_0(x_0, y_0, \rho) &= \tilde{t}_{01}(x_0) \cdot \tilde{t}_{02}''(y_0) = \\ &t_{01} \cdot t_{02} + t_{02} t_1 \cos(2\pi f_1 x_0) + t_{01} t_2 \cos(2\pi f_2 x_0) + \\ &\frac{1}{2} t_1 t_2 \cos[2\pi(f_1 x_0 + f_2 y_0)] + \\ &\frac{1}{2} t_1 t_2 \cos[2\pi(f_1 x_0 - f_2 y_0)] \end{aligned} \quad (3)$$

把(1)式和(2)式代入(3)式计算时,取 $\varphi_0 = \varphi_0' = 0$ 。

薄透镜的变换函数形式为^[2-9]:

$$\tilde{t}_{03}(x_0, y_0, \rho) = \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \quad (4)$$

正交余弦光栅和透镜组合在一起的变换函数为:

$$\tilde{t}(x_0, y_0, \rho) = \tilde{t}_0(x_0, y_0, \rho) \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \quad (5)$$

当用波长为 λ 、振幅为 A_0 的一束平行光照射这正交余弦光栅时,则出射光波前为:

$$\tilde{U}_2(x_0, y_0, \rho) = A_0 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \cdot$$

$$\begin{aligned} &\{ [t_{01} \cdot t_{02} + t_{02} t_1 \cos(2\pi f_1 x_0) + t_{01} t_2 \cos(2\pi f_2 x_0) + \\ &\frac{1}{2} t_1 t_2 \cos[2\pi(f_1 x_0 + f_2 y_0)] + \\ &\frac{1}{2} t_1 t_2 \cos[2\pi(f_1 x_0 - f_2 y_0)] \} \quad (6) \end{aligned}$$

由此可见,它相当于是由 4 个余弦光栅和一个单缝组成的光学衍射系统。则(6)式可看成球面波照射到 4 个余弦光栅和单缝所组成的衍射系统上。

设 $\gamma_1 = \frac{t_1}{t_{01}}, \gamma_2 = \frac{t_2}{t_{02}}, A_1 = A_0 t_{01} t_{02}$ (γ 可称其为振幅衬比度,其取值范围为 $0 < \gamma \leq 1$),由欧拉公式得出这波前包含 9 种成分:

$$\begin{aligned} \tilde{U}_0(x_0, y_0, \rho) &= A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right), \tilde{U}_{+1}(x_0, y_0, \rho) = \\ &\frac{\gamma_1}{2} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp(i2\pi f_1 x_0), \tilde{U}_{-1}(x_0, y_0, \rho) = \\ &\frac{\gamma_1}{2} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp(-i2\pi f_1 x_0), \tilde{U}_{+2}(x_0, y_0, \rho) = \\ &\frac{\gamma_2}{2} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp(i2\pi f_2 y_0), \tilde{U}_{-2}(x_0, y_0, \rho) = \\ &\frac{\gamma_2}{2} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp(-i2\pi f_2 y_0), \tilde{U}_{+3}(x_0, y_0, \rho) = \\ &\frac{\gamma_1 \gamma_2}{4} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp[i2\pi(f_1 x_0 + f_2 y_0)], \\ \tilde{U}_{-3}(x_0, y_0, \rho) &= \frac{\gamma_1 \gamma_2}{4} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \times \\ &\exp[-i2\pi(f_1 x_0 + f_2 y_0)], \tilde{U}_{+4}(x_0, y_0, \rho) = \frac{\gamma_1 \gamma_2}{4} A_1 \times \\ &\exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp[i2\pi(f_1 x_0 - f_2 y_0)], \tilde{U}_{-4}(x_0, y_0, \rho) = \\ &\frac{\gamma_1 \gamma_2}{4} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \exp[-i2\pi(f_1 x_0 - f_2 y_0)] \end{aligned}$$

用波前相因子判断法得出 $\tilde{U}_0(x_0, y_0, \rho), \tilde{U}_{+1}(x_0, y_0, \rho), \tilde{U}_{-1}(x_0, y_0, \rho), \tilde{U}_{+2}(x_0, y_0, \rho), \tilde{U}_{-2}(x_0, y_0, \rho), \tilde{U}_{+3}(x_0, y_0, \rho), \tilde{U}_{-3}(x_0, y_0, \rho), \tilde{U}_{+4}(x_0, y_0, \rho), \tilde{U}_{-4}(x_0, y_0, \rho)$ 这 9 种基元成分为 9 列会聚球面波,它们分别会聚于衍射屏 $P_0, P_{+1}, P_{+2}, P_{+3}, P_{+4}, P_{-1}, P_{-2}, P_{-3}, P_{-4}$ 处,如图 3 所示。然而,事情的复杂性来自于正交余弦光栅有限孔径的影响。

在傍轴条件下,近似处理振幅传播因子,取 $\frac{1}{r} \approx$

$\frac{1}{z}, ds = dx_0 dy_0$, 根据菲涅耳-基尔霍夫衍射积分表达式得到 9 列会聚球面波的衍射波前函数:

$$\tilde{U}_0(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} A_1 \exp\left(-ik \frac{x_0^2 + y_0^2}{2z_0}\right) \times$$

$$\exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{+1}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_1}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp(i2\pi f_1 x_0) \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{-1}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_1}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp(-i2\pi f_1 x_0) \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{+2}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_2}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp(i2\pi f_2 y_0) \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{-2}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_2}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp(-i2\pi f_2 y_0) \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{+3}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_2}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \exp[i2\pi(f_1 x_0 + f_2 y_0)] \times$$

$$\exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{-3}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_2}{2} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp[-i2\pi(f_1 x_0 + f_2 y_0)] \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{+4}(x, y, z) = -\frac{i}{\lambda z} \iint_{\Sigma_0} \frac{\gamma_1 \gamma_2}{4} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \times$$

$$\exp[i2\pi(f_1 x_0 - f_2 y_0)] \exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0,$$

$$\bar{U}_{-4}(x, y, z) = -\frac{i}{\lambda z} \times$$

$$\iint_{\Sigma_0} \frac{\gamma_1 \gamma_2}{4} A_1 \exp \left(-ik \frac{x_0^2 + y_0^2}{2z_0} \right) \exp[-i2\pi(f_1 x_0 - f_2 y_0)] \times$$

$$\exp \left[ik \left(z + \frac{x_0^2 + y_0^2}{2z} + \frac{x^2 + y^2}{2z} - \frac{xx_0 + yy_0}{z} \right) \right] dx_0 dy_0.$$

上面的积分号内都含有 x_0, y_0 2 次项因子和 1 次项因子,使得积分运算相当繁杂,难以用简单的解析函数表达出来。若只考虑像面上的衍射,问题就简单了。

4 正交余弦光栅在像面的衍射场

取 $z = z_0$,由上面 9 个积分式得正交余弦光栅在像面衍射的波前函数为:

$$U(x, y, z_0) = \left\{ \left[\text{sinc} \left(k \frac{x}{z_0} \frac{a}{2} \right) + \frac{\gamma_1}{2} \text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) + \frac{\gamma_1}{2} \text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \right] \text{sinc} \left(k \frac{y}{z_0} \frac{b}{2} \right) + \frac{\gamma_2}{2} \text{sinc} \left(k \frac{x}{z_0} \frac{a}{2} \right) \times \right.$$

$$\left. \left[\text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \frac{\gamma_2}{2} \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) \right] + \frac{\gamma_1 \gamma_2}{4} \times \right.$$

$$\left. \left[\text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) \right] + \right.$$

$$\left. \frac{\gamma_1 \gamma_2}{4} \left[\text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) \right] \right\} A_2 e^{i\varphi} \quad (7)$$

式中 $A_2 = \frac{A_1 ab}{\lambda z_0}$, $\varphi = kz_0 + k \frac{x^2 + y^2}{2z_0} - \frac{\pi}{2}$ 。

根据 (7) 式得正交余弦光栅在 $z = z_0$ 处,衍射振幅分布函数(取正值)和光强分布函数为:

$$A(x, y, z_0) = A_2 \left[\text{sinc} \left(k \frac{x}{z_0} \frac{a}{2} \right) + \frac{\gamma_1}{2} \text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) + \frac{\gamma_1}{2} \text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \right] \text{sinc} \left(k \frac{y}{z_0} \frac{b}{2} \right) +$$

$$\frac{\gamma_2}{2} \text{sinc} \left(k \frac{x}{z_0} \frac{a}{2} \right) \left[\text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \frac{\gamma_2}{2} \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) \right] +$$

$$\frac{\gamma_1 \gamma_2}{4} \left[\text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) + \right.$$

$$\left. \frac{\gamma_1 \gamma_2}{4} \left[\text{sinc} \left(k \left(\lambda f_1 + \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 - \frac{y}{z_0} \right) \frac{b}{2} \right) + \text{sinc} \left(k \left(\lambda f_1 - \frac{x}{z_0} \right) \frac{a}{2} \right) \text{sinc} \left(k \left(\lambda f_2 + \frac{y}{z_0} \right) \frac{b}{2} \right) \right] \right] \quad (8)$$

$$\begin{aligned}
 I(x, y, z_0) = I_0 & \left\{ \left[\operatorname{sinc}\left(k \frac{x}{z_0} \frac{a}{2}\right) + \frac{\gamma_1}{2} \operatorname{sinc}\left(k\left(\lambda f_1 - \frac{x}{z_0}\right) \frac{a}{2}\right) + \frac{\gamma_1}{2} \operatorname{sinc}\left(k\left(\lambda f_1 + \frac{x}{z_0}\right) \frac{a}{2}\right) \right] \operatorname{sinc}\left(k \frac{y}{z_0} \frac{b}{2}\right) + \right. \\
 & \left. \frac{\gamma_2}{2} \operatorname{sinc}\left(k \frac{x}{z_0} \frac{a}{2}\right) \left[\operatorname{sinc}\left(k\left(\lambda f_2 - \frac{y}{z_0}\right) \frac{b}{2}\right) + \frac{\gamma_2}{2} \operatorname{sinc}\left(k\left(\lambda f_2 + \frac{y}{z_0}\right) \frac{b}{2}\right) \right] + \right. \\
 & \frac{\gamma_1 \gamma_2}{4} \left[\operatorname{sinc}\left(k\left(\lambda f_1 - \frac{x}{z_0}\right) \frac{a}{2}\right) \operatorname{sinc}\left(k\left(\lambda f_2 - \frac{y}{z_0}\right) \frac{b}{2}\right) + \operatorname{sinc}\left(k\left(\lambda f_1 + \frac{x}{z_0}\right) \frac{a}{2}\right) \operatorname{sinc}\left(k\left(\lambda f_2 + \frac{y}{z_0}\right) \frac{b}{2}\right) + \right. \\
 & \left. \left. \frac{\gamma_1 \gamma_2}{4} \left[\operatorname{sinc}\left(k\left(\lambda f_1 + \frac{x}{z_0}\right) \frac{a}{2}\right) \operatorname{sinc}\left(k\left(\lambda f_2 - \frac{y}{z_0}\right) \frac{b}{2}\right) + \operatorname{sinc}\left(k\left(\lambda f_1 - \frac{x}{z_0}\right) \frac{a}{2}\right) \operatorname{sinc}\left(k\left(\lambda f_2 + \frac{y}{z_0}\right) \frac{b}{2}\right) \right] \right\}^2 \quad (9)
 \end{aligned}$$

式中 $I_0 = A_2^2 = \left(\frac{A_1 ab}{\lambda z_0}\right)^2$ 。

根据 (8) 式和 (9) 式得到相面上振幅和光强的分布图,如图 4 和图 5 所示。相关参量取值为: $\lambda = 630\text{nm}$, $z_0 = 0.4\text{m}$, $\gamma_1 = 0.8$, $\gamma_2 = 0.8$, $A_1 = 1$, $\lambda f_2 = 0.01$, $\lambda f_1 = 0.005$, $a = 20\text{mm}$, $b = 20\text{mm}$ 。

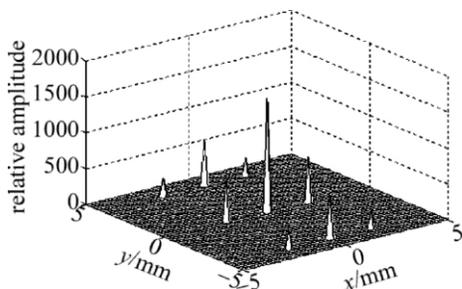


Fig. 4 Amplitude distribution of diffraction fields

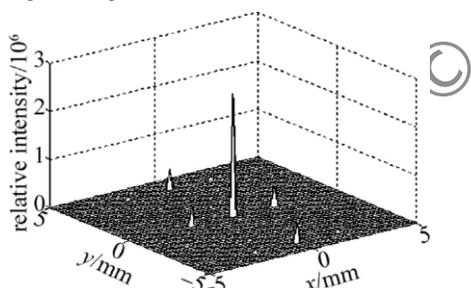


Fig. 5 Light distribution of diffraction fields

对于光栅的衍射,以往多有研究文献发表^[10-13],本文中以正交余弦光栅为轴对称的衍射屏为研究对象,揭示其衍射场所含成分,即 1 列平面衍射波和 8 列球面衍射波。从图 4 和图 5 中可以看出,在 P_0 点左右的轴向区间,会聚球面波 $\tilde{U}_0(x, y, z_0)$ 项是主要贡献者;在 P_{+1} 点左右的轴向区间,会聚球面衍射波 $\tilde{U}_{+1}(x, y, z_0)$ 项是主要贡献者。

考虑到正交余弦光栅孔径的限制,根据 (8) 式还可以得到中心主斑点的半角宽度为: $\Delta\theta_{0x} \approx \frac{\lambda}{a}$, $\Delta\theta_{0y} \approx \frac{\lambda}{b}$ 。

5 结论

以上分析方法和半波带、矢量法相比较^[14-16],问题更加严密直观,克服了半波带法和矢量法的半定量、

半定性分析方法的不足,并且所得结果和实验结果是一致的。

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